

- 3.14** The material dispersion in an optical fiber defined by $|d^2n_1/d\lambda^2|$ is $4.0 \times 10^{-2} \mu\text{m}^{-2}$. Estimate the pulse broadening per kilometre due to material dispersion within the fiber when it is illuminated with an LED source with a peak wavelength of $0.9 \mu\text{m}$ and an rms spectral width of 45 nm .
- 3.15** Describe the mechanism of intermodal dispersion in a multimode step index fiber. Show that the total broadening of a light pulse δT_s due to intermodal dispersion in a multimode step index fiber may be given by:

$$\delta T_s \approx \frac{L(NA)^2}{2n_1c}$$

where L is the fiber length, NA is the numerical aperture of the fiber, n_1 is the core refractive index and c is the velocity of light in a vacuum.

A multimode step index fiber has a numerical aperture of 0.2 and a core refractive index of 1.47 . Estimate the bandwidth-length product for the fiber assuming only intermodal dispersion and a return to zero code when:

- (a) there is no mode coupling between the guided modes;
- (b) mode coupling between the guided modes gives a characteristic length equivalent to 0.6 of the actual fiber length.
- 3.16** Using the relation for δT_s given in Problem 3.15, derive an expression for the rms pulse broadening due to intermodal dispersion in a multimode step index fiber. Compare this expression with a similar expression which may be obtained for an optimum near parabolic profile graded index fiber. Estimate the bandwidth-length product for the step index fiber specified in Problem 3.15 considering the rms pulse broadening due to intermodal dispersion within the fiber and comment on the result. Indicate the possible improvement in the bandwidth-length product when an optimum near parabolic profile graded index fiber with the same relative refractive index difference and core axis refractive index is used. In both cases assume only intermodal dispersion within the fiber and the use of a return to zero code.
- 3.17** An 11 km optical fiber link consisting of optimum near parabolic profile graded index fiber exhibits rms intermodal pulse broadening of 346 ps over its length. If the fiber has a relative refractive index difference of 1.5% , estimate the core axis refractive index. Hence determine the numerical aperture for the fiber.
- 3.18** A multimode, optimum near parabolic profile graded index fiber has a material dispersion parameter of $30 \text{ ps nm}^{-1} \text{ km}^{-1}$ when used with a good LED source of rms spectral width 25 nm . The fiber has a numerical aperture of 0.4 and a core axis refractive index of 1.48 . Estimate the total rms pulse broadening per kilometre within the fiber assuming waveguide dispersion to be negligible. Hence, estimate the bandwidth-length product for the fiber.
- 3.19** A multimode step index fiber has a relative refractive index difference of 1% and a core refractive index of 1.46 . The maximum optical bandwidth that may be obtained with a particular source on a 4.5 km link is 3.1 MHz .
- (a) Determine the rms pulse broadening per kilometre resulting from intramodal dispersion mechanisms.
- (b) Assuming waveguide dispersion may be ignored, estimate the rms spectral width of the source used, if the material dispersion parameter for the fiber at the operating wavelength is $90 \text{ ps nm}^{-1} \text{ km}^{-1}$.

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- 3.20 Describe the phenomenon of modal noise in optical fibers and suggest how it may be avoided.
- 3.21 Discuss dispersion mechanisms with regard to single-mode fibers indicating the dominating effects. Hence, describe how intramodal dispersion may be minimized within the single-mode region.
- 3.22 An approximation for the normalized propagation constant in a single-mode step index fiber shown in Example 2.9 is:

$$b(V) \approx \left(1.1428 - \frac{0.9960}{V} \right)^2$$

Obtain a corresponding approximation for the waveguide parameter $V d^2(Vb)/dV^2$ and hence write down an expression for the waveguide dispersion in the fiber.

Estimate the waveguide dispersion in a single-mode step index fiber at a wavelength $1.34 \mu\text{m}$ when the fiber core radius and refractive index are $4.4 \mu\text{m}$ and 1.48 respectively.

- 3.23 A single-mode step index fiber exhibits material dispersion of $7 \text{ ps nm}^{-1} \text{ km}^{-1}$ at an operating wavelength of $1.55 \mu\text{m}$. Using the approximation obtained in Problem 3.22, estimate the fiber core diameter which will enable the waveguide dispersion to cancel the material dispersion so that zero intramodal dispersion is obtained at this wavelength. The refractive index of the fiber core is 1.45 .
- 3.24 A single-mode step index fiber has a zero-dispersion wavelength of $1.29 \mu\text{m}$ and exhibits total first order dispersion of $3.5 \text{ ps nm}^{-1} \text{ km}^{-1}$ at a wavelength of $1.32 \mu\text{m}$. Determine the total first order dispersion in the fiber at a wavelength of $1.54 \mu\text{m}$.
- 3.25 Describe the techniques employed and the fiber structures utilized to provide:
- dispersion shifted single-mode fibers;
 - dispersion flattened single-mode fibers.

- 3.26 Explain what is meant by:

- modal birefringence;
- the beat length;

in single-mode fibers.

The difference between the propagation constants for the two orthogonal modes in a single-mode fiber is 250 . It is illuminated with light of peak wavelength $1.55 \mu\text{m}$ from an injection laser source with a spectral linewidth of 0.8 nm . Estimate the coherence length within the fiber.

- 3.27 The difference in the effective refractive indices ($n_x - n_y$) for the two orthogonally polarized modes in conventional single-mode fibers are in the range $9.3 \times 10^{-7} < n_x - n_y < 1.1 \times 10^{-5}$. Determine the corresponding range for the beat lengths of the fibers when they are operating at a transmission wavelength of $1.3 \mu\text{m}$. Hence obtain the range of the modal birefringence for the fibers.
- 3.28 A single-mode fiber maintains birefringent coherence over a length of 100 km when it is illuminated with an injection laser source with a spectral linewidth of 1.5 nm and a peak wavelength of $1.32 \mu\text{m}$. Estimate the beat length within the fiber and comment on the result.
- 3.29 Provide a definition for polarization mode dispersion in single-mode optical fibers.
The maximum bit rate that can be achieved over a 6 km length of highly birefringent

single-mode fiber is 400 kbits^{-1} . Assuming polarization mode dispersion to be the dominant dispersive mechanism, calculate its value within this fiber.

- 3.30 Describe, with the aid of sketches, the techniques that can be employed to produce both high and low birefringence PM fibers.

A two polarization mode PM fiber has a mode coupling parameter of $2.3 \times 10^{-5} \text{ m}^{-1}$ when operating at a wavelength of $1.55 \mu\text{m}$. Estimate the polarization crosstalk for the fiber at this wavelength.

- 3.31 Explain what is meant by self phase modulation.

Identify and discuss a major application area for this nonlinear phenomenon.

Answers to numerical problems

- | | | | |
|------|---|------|--|
| 3.1 | 57.5 km | 3.16 | 15.3 MHz km; improvement to
10.9 GHz km |
| 3.2 | $10.0 \mu\text{W}$ | 3.17 | 1.45, 0.25 |
| 3.3 | $703 \mu\text{W}$ | 3.18 | 774 ps km^{-1} , 258 MHz km |
| 3.5 | 1.57 dB km^{-1} , 0.14 dB km^{-1} | 3.19 | (a) 2.82 ns km^{-1} ; (b) 31 nm |
| 3.6 | 1.49 | 3.22 | $-3.92 \text{ ps nm}^{-1} \text{ km}^{-1}$ |
| 3.7 | $1.50 \mu\text{m}$, 0.30 dB km^{-1} | 3.23 | $7.2 \mu\text{m}$ |
| 3.8 | 2.4 W | 3.24 | $23.6 \text{ ps nm}^{-1} \text{ km}^{-1}$ |
| 3.9 | $0.86 \mu\text{m}$ | 3.26 | 48.6 m |
| 3.10 | 0.47% | 3.27 | $12 \text{ cm} < L_B < 1.4 \text{ m}$;
$9.3 \times 10^{-7} < B_T < 1.1 \times 10^{-5}$ |
| 3.11 | (a) 13.2 MHz km; (b) 800 ps | 3.28 | 113.6 m |
| 3.12 | (a) 10 ns; (b) 4 ns | 3.29 | 682 ps km^{-1} |
| 3.13 | 1.2 ns | 3.30 | -16.4 dB km^{-1} |
| 3.14 | 5.4 ns km^{-1} | | |
| 3.15 | (a) 11.0 MHz km; (b) 14.2 MHz km | | |

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